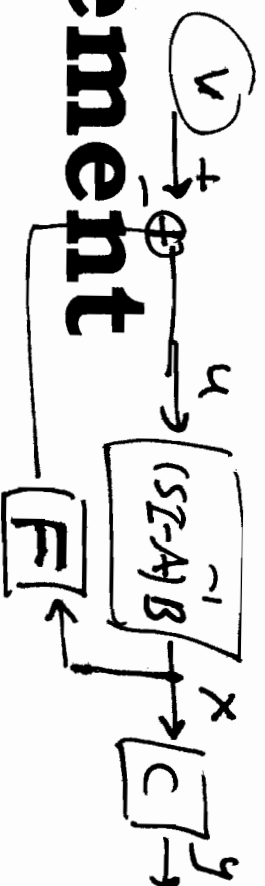


# Pole Placement



- Choose  $F$  based on the desired closed loop characteristic polynomials.

$$f_1 = a_{a_0} - a_0, f_2 = a_{a_1} - a_1, \dots, f_n = a_{a_{n-1}} - a_{n-1}$$

$$\dot{x} = Ax + Bu \quad \text{Example: } G(s) = 1/(s^2 + 2.427s)$$

$$= (A - BF)x + Bu$$

$$A = \begin{bmatrix} 0 & 1 \\ 0 & -2.427 \end{bmatrix} \quad B = \begin{bmatrix} 0 \\ 1 \end{bmatrix}$$

$$Y = Cx$$

Desired poles at (-10, -15)

Desired closed loop characteristic poly:

$$s^2 + 25s + 150$$

$$F = [150 \quad 25 - 2.427] = [150 \quad 22.573]$$

$\text{eig}(A) = \text{open loop poles}$

$$\dot{x} = Ax + Bu$$

~~$$Y = Cx$$~~

Suppose  $x$  is available

(full state feedback)

Linear full state feedback

$$u = -Fx$$

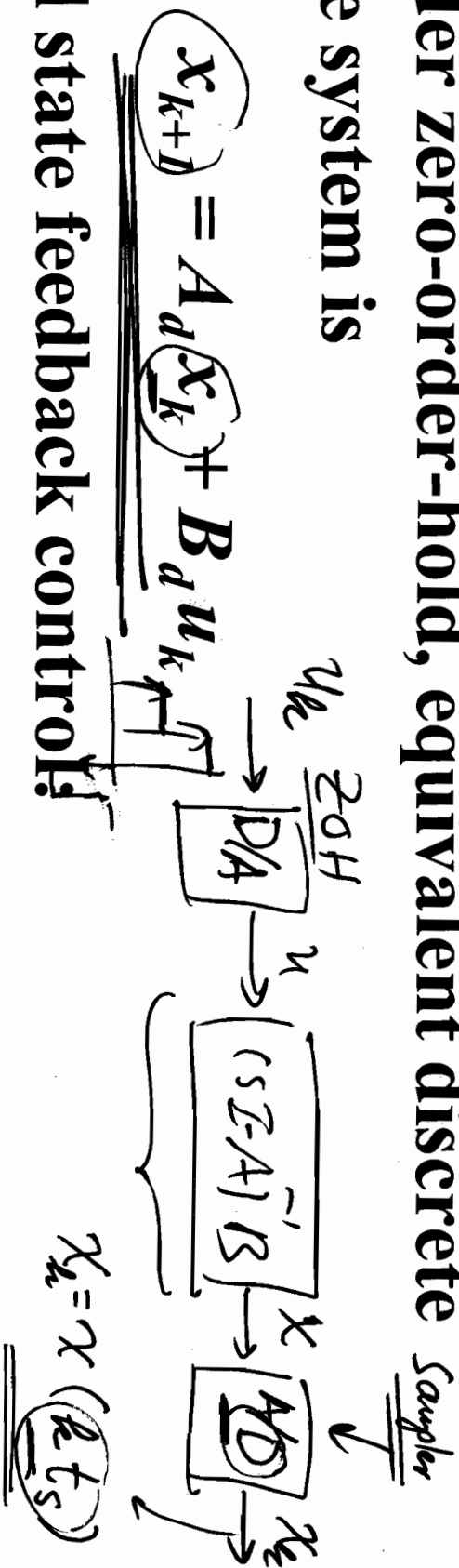
Closed loop eigenvalues

$$\dot{x} = (A - BF)x$$

- MATLAB tools: place, acker**

# Discrete Time Systems

Under zero-order-hold, equivalent discrete time system is



Full state feedback control:

$$u_k = -F(x_k - x_d)$$

$t_s = \text{Sampling period}$

Pole placement can again be used to place the closed loop poles  $\text{eig}(A_d - B_d F)$  within the unit circle.

# Full State Observer

$$\dot{\hat{x}} = \underbrace{A\hat{x} + Bu}_{\text{replica of plant}} - L \left( \underbrace{C\hat{x} + Du}_{\text{estimated output}} - \underbrace{y}_{\text{output estimation error}} \right) \quad \overset{Cx+Du}{\cancel{}} \quad \hat{x}(0) = 0$$

correction based on  
output estimation error

$$\dot{x} = Ax + Bu \quad x(0) = x_0$$

$$\dot{x} - \dot{\hat{x}} = A(x - \hat{x}) + L(-C(x - \hat{x}))$$

$$e_x \triangleq x - \hat{x}$$

$$x(0) - \hat{x}(0) = x_0$$

$$\dot{e}_x = (A - LC)e_x \quad e_x(0) = x_0$$

## How do we choose $L$ ?

Fact:  $\text{eig}(A) = \text{eig}(A^T)$

$$(A - LC)^T = A^T - (LC)^T$$

Therefore,  $\text{eig}(A - LC) = \text{eig}(A^T - C^T L^T) = A^T - C^T L^T$

This is exactly the same as the full state

feedback case except  $(A, B)$  is replaced by

$$(A^T, C^T).$$

Rule of Thumb: Observer poles should be 5-

10 times faster than the controller poles.

$$\dot{x} = Ax + Bw(t); x(0) = x_0$$

zero input solution:

$$\dot{x} = Ax; x(0) = x_0$$

Scalar

$$x = e^{At} x_0$$

$$\sum_{i=0}^{\infty} \frac{A^i t^i}{i!} x_0$$

$$x = e^{At} x_0$$

$$x = e^{At} x_0$$

$$\sum_{i=0}^{\infty} \frac{A^i t^i}{i!}$$

Verify:  $\frac{d}{dt} e^{At} = A e^{At}$

$$e^{At} \Big|_{t=0} = I$$

Zero state solution

$$x = Ax + B \delta(t)$$

$$\dot{x} - Ax = B \delta(t)$$

$$e^{-At} (\dot{x} - Ax)$$

$$= e^{-At} B \delta(t)$$

$$= -A e^{-At} x(t) + e^{-At} \dot{x}(t)$$

commute

$$= e^{-At} (\dot{x}(t) - Ax(t))$$

$$\frac{d}{dt} (e^{-At} x(t)) = e^{-At} B \delta(t)$$

Integrate both sides:

$$e^{-At} x(t) = \int_t^0 e^{-Az} B \delta(z) dz$$

$$= B$$

$$\therefore \underline{\underline{x(t) = e^{At} B}}$$

impulse response

Complete response of

$$\dot{x} = Ax + Bu \quad x(0) = x_0$$

$$x(t) = e^{At} x_0 + \int_0^t e^{A(t-\tau)} B u(\tau) d\tau$$

zero input

convolution between zero state response & input

$$x((k+1)T_s) = e^{A T_s} x(kT_s) + \int_{t_s}^0 e^{A(t_s-\tau)} B u(\tau) d\tau$$

$$= e^{A T_s} x(kT_s) + \int_{t_s}^0 e^{A(t_s-\tau)} B u(\tau) d\tau$$

$$x_{k+1} = A x_k + B u_k$$

$x_0, a x_0, a^2 x_0, a^3 x_0$

$$+ \int_{t_s}^0 e^{A(t_s-\tau)} B u(\tau) d\tau$$

eigenvalues

$$x_{k+1} = A_d x_k + B_d u_k = (A_d - B_d F) x_k + B_d u_k$$

$u_k = -F x_k$

$$\dot{\hat{x}} = (A - BF - LC) \hat{x} + Ly$$

$$u = -F \hat{x}$$

$$\dot{\hat{x}} = A \hat{x} + Bu - L(C \hat{x} - y)$$

$$u = -F \hat{x}$$



Controller